

Thesis/
Reports
Pellerin,
R.F.

Research Report No. 79/57-19

EVALUATION OF DIMENSION LUMBER
MADE FROM DEAD TREES



COLLEGE OF ENGINEERING
RESEARCH DIVISION

COLLEGE OF ENGINEERING
RESEARCH DIVISION

Research Report No. 79/57-19

EVALUATION OF DIMENSION LUMBER
MADE FROM DEAD TREES

May 1979

Project No. 11D-3857

Roy F. Pellerin
Roy F. Pellerin

Contract No. 1799

Sponsor Project No. 12-11-204-13

Sponsor Contract No.

Washington State University

Pullman, Washington

EVALUATION OF DIMENSION LUMBER
MADE FROM DEAD TREES

Final Report

to

U.S. Forest Service
Intermountain Forest & Range Experiment Station
Ogden, Utah 84401

May 1979

by

Roy F. Pellerin
Wood Technology Section
Department of Materials Science & Engineering
Washington State University
Pullman, Washington 99164

EVALUATION OF DIMENSION LUMBER
MADE FROM DEAD TREES

INTRODUCTION

The Inland Empire area contains an abundant supply of dead trees, the result of current and past insect and disease epidemics. Some of these trees are being harvested as a component of ongoing timber sales and the logs are mixed with the green logs for processing. Accordingly the lumber from the dead trees is mixed with green tree lumber for sale and use. As more and more of these trees are utilized, information is needed as to the effect of the exposure conditions on the mechanical properties of the lumber cut from these trees.

Since lumber is used normally for construction where strength properties are often of primary consideration, the effect of death, subsequent exposure and utilization on the mechanical perproperties of dead tree lumber is an urgent need. Nondestructive testing methods have been developed at Washington State University and have been used to evaluate log and lumber quality (1,5). The results of these studies verify that the procedure successfully measures modulus of elasticity from which corresponding values of modulus of rupture can be assigned.

OBJECTIVES

The objectives of this study are: to obtain nondestructive test data for dimension lumber from dead trees of two species, lodgepole pine and western white pine; to test to failure or a sample of the study lumber; to establish the relationship between nondestructive and destructive test values and to compare the results obtained from the dead tree lumber with similar data obtained in previous studies on green tree dimension lumber.

PROCEDURE

Dimension lumber from two species, lodgepole pine and western white pine, was used in the study. The lodgepole pine was obtained from a cooperating sawmill in Montana and the western white pine from a sawmill in Idaho.

The mills were requested to segregate a representative sample of logs obtained from trees that have been dead for various intervals of time. The sample logs were sawn consecutively in a short mill run. The logs were also processed through the mill in accordance with the mill's standard procedure, however, the production of 2 by 4's and 2 by 6's, 10, 12 and 14 feet long were favored. The lodgepole pine dimension lumber cut from the sample logs was segregated at the green chain and set aside for shipment to Washington State University. The western white pine dimension lumber was kiln dried, surfaced, visually graded and segregated so that approximately equal numbers of each grade were obtained for the study. A breakdown of lumber grade, size and quantity is shown in Table I.

Table I. Description of Lumber Selected for Analysis.

Species	Size	Length	Number
Lodgepole pine	2 x 4	8 ft	3
		10 ft	20
		12 ft	40
		14 ft	27
		16 ft	20
	2 x 6	10 ft	8
		12 ft	12
		14 ft	10
		16 ft	8
White pine	2 x 4	8 ft	4
		10 ft	18
		12 ft	47
		14 ft	57
		16 ft	112

Upon receipt at Washington State University the lodgepole pine lumber was stickered, air-dried and surfaced prior to subsequent testing. The western white pine, having already been kiln dried and surface^d/was stickered and allowed to reach equilibrium prior to further testing.

A recent study by Lowery and Hearst (3) indicated that the average moisture content of lodgepole pine lumber from dead trees is approximately 16.5 percent and for western white pine the average is approximately 24 percent. The moisture content of the study lumber at the time of testing was 6 to 7 percent.

After conditioning, each board was nondestructively evaluated with both the E-Computer and the stress wave equipment. Both of these nondestructive methods were developed at Washington State University.

The E-Computer computes the modulus of elasticity of a board from its resonant frequency while supported near its ends. The longitudinal stress wave method determines the modulus of elasticity of a board from the velocity of propagation of a stress wave passing longitudinally through the board and the density of the board.

After nondestructive evaluation, each board was tested on edge to failure in flexure according to ASTM D-198 standards.

RESULTS AND DISCUSSION

Lodgepole Pine

The data obtained from each lodgepole pine specimen is recorded in Appendix A. Besides the values for nondestructive and static properties the data includes dimensions, weight, moisture content at time of test, and the visual grade for each specimen. Table II contains a summary of the regression analysis for each size and combination of properties for the lodgepole pine specimens.

Table II. Analysis of Data for Lodgepole Pine

Size	Abscissa	Ordinate	Number of Specimens	Regression Equation	Correlation Coefficient	Correlation of Determination
2 x 6	E-Computer	E-Stress wave	38	E-stress wave = -0.038 + 1.237 E-computer	0.95	0.90
	E-Computer	E-Static	38	E-static = -0.036 + 0.976 E-computer	0.87	0.76
	E-Computer	MOR	38	MOR = -632.9 + 4067 E-computer	0.68	0.46
	E-Stress wave	E-Static	38	E-Static = 0.059 + 0.75 E-stress wave	0.87	0.76
	E-Stress wave	MOR	38	MOR = -578.4 + 3328.9 E-stress wave	0.73	0.53
2 x 4	E-Computer	E-Stress wave	110	E-stress wave = 0.132 + 1.106 E-computer	0.94	0.88
	E-Computer	E-Static	110	E-static = -0.130 + 1.068 E-computer	0.87	0.76
	E-Computer	MOR	110	MOR = -2597.1 + 6174.65 E-computer	0.71	0.51
	E-Stress wave	E-Static	110	E-static = -0.093 + 0.860 E-stress wave	0.83	0.69
	E-Stress wave	MOR	110	MOR = -2158.2 + 4829.586 E-stress wave	0.66	0.43

Western White Pine

The data obtained from each western white pine specimen is recorded in Appendix B. Besides the values for nondestructive and static properties the data includes dimensions, weight, moisture content at time of test, and the visual grade for each specimen. Table III contains a summary of the regression analysis for each combination of properties for the western white pine specimens.

Green Tree Lumber

Data obtained from previous studies on green tree lumber was used for comparison purposes with the dead tree lumber studied in this research. Table III contains a summary of the regression analysis for each combination of properties for green tree lumber. Previous studies, of course, were not conducted exactly like this study. Therefore, Table IV is made up of more than one study.

The 2 x 8 and 2 x 6 green tree lumber has been extracted from reports by G. G. Marra, et al (4) and R. F. Pellerin (6). The 2 x 4 green tree lumber has been extracted from a study by R. J. Hoyle (2) on 1.5E 1650 f MSR graded hem-fir.

Past experience in research on nondestructive testing of wood shows us that variation due to species is minimal.

Graphs of the regression lines of the various species, sizes, and soundness of lumber for E-computer versus E-static and E-computer versus E-stress wave are presented in Figures I and II respectively.

In Figure I, the regression lines for the 2 x 4 and 2 x 6 dead lodge-pole pine groups well with the 2 x 6 green lumber regression line and line for the 2 x 4 dead white pine corresponds well with that for the 2 x 4

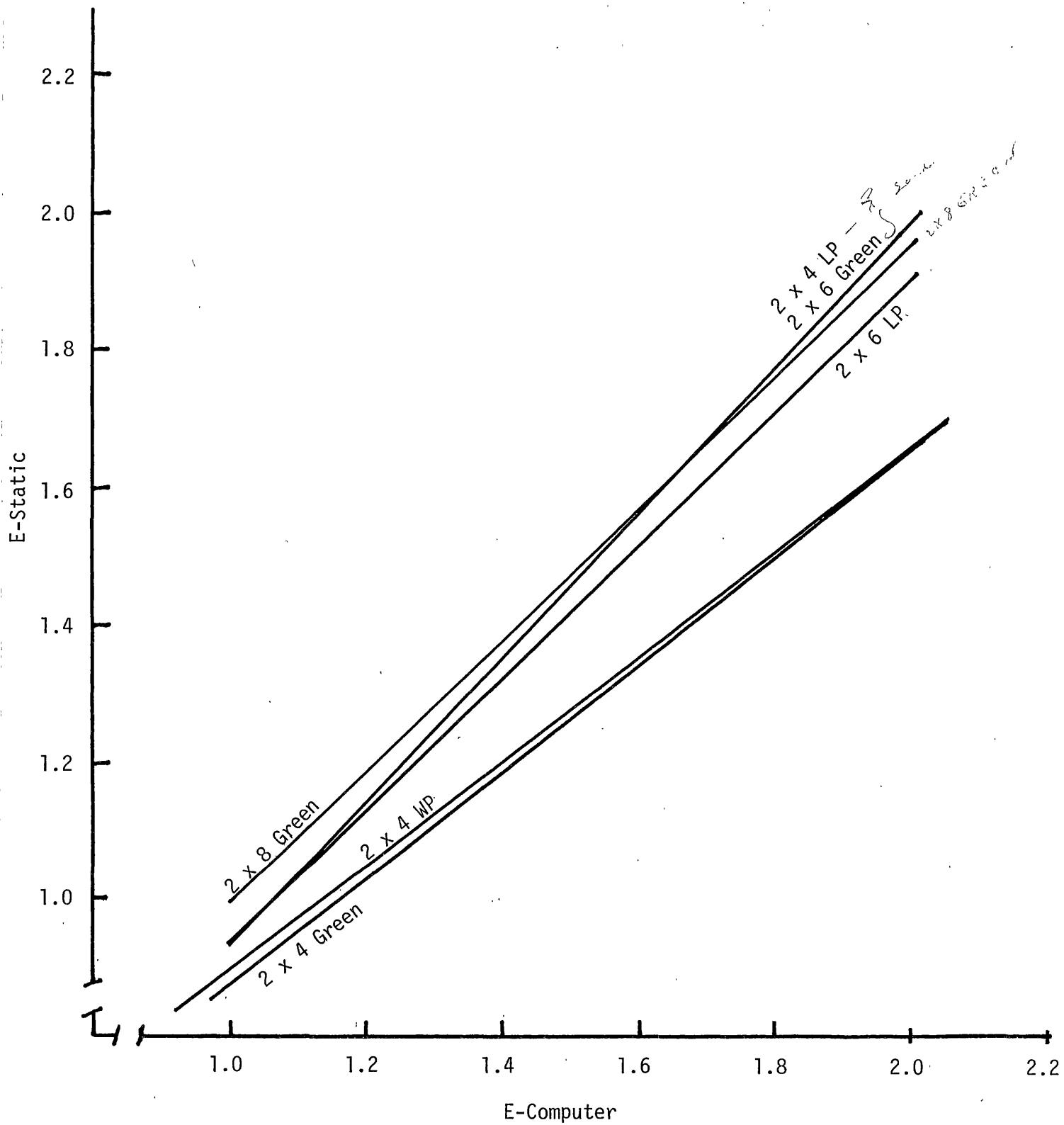


Figure I.

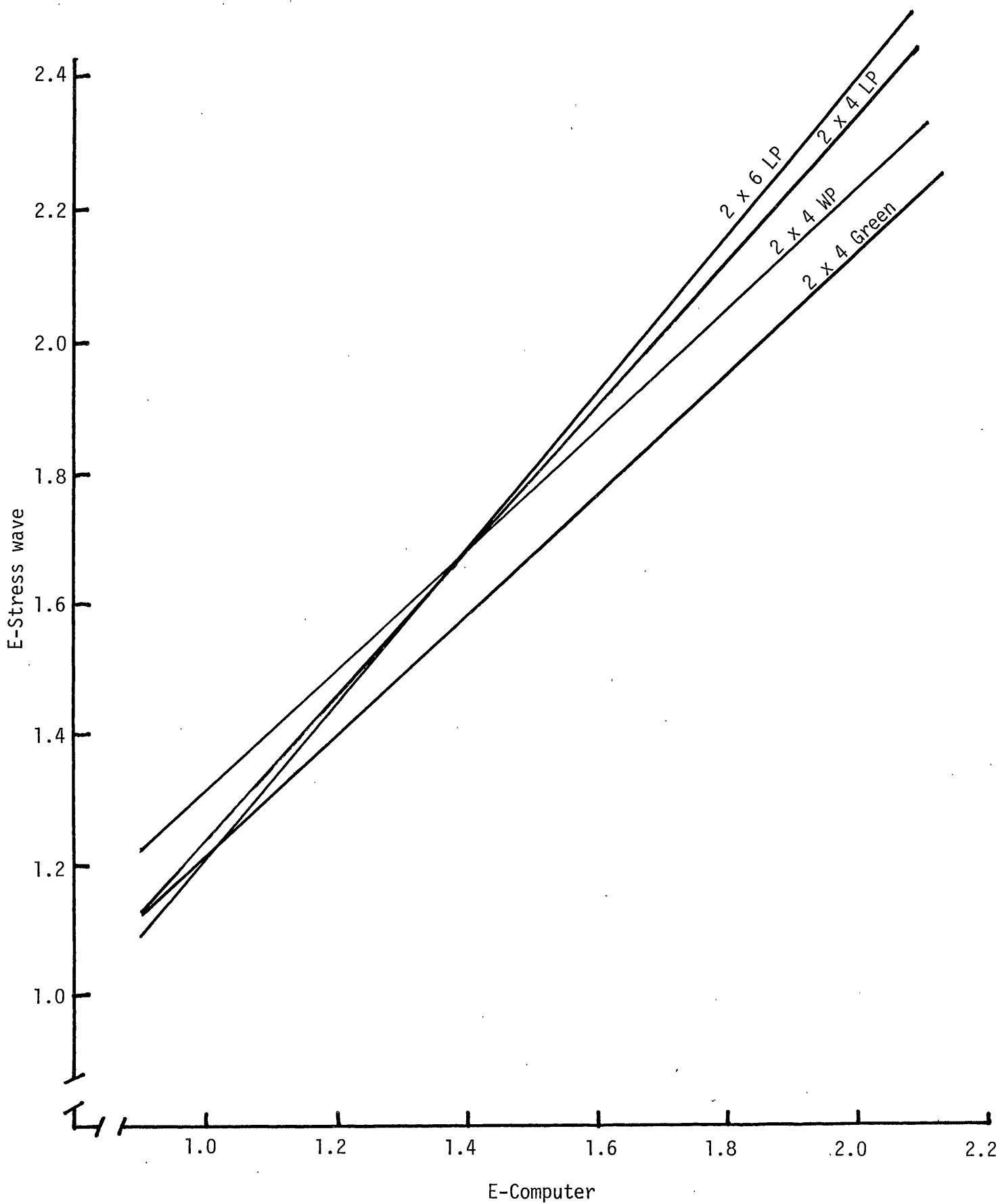


Figure II.

Table III. Analysis of Data for Western White Pine.

Size	Abscissa	Ordinate	Number of Specimens	Regression Equation	Correlation Coefficient	Coefficient of Determination
2 x 4	E-Computer	E-Stress wave	238	E-stress wave = 0.417 + 0.906 E-computer	0.90	0.81
	E-Computer	E-Static	238	E-static = 0.148 + 0.756 E-computer	0.80	0.64
	E-Computer	MOR	238	MOR = -1063.2 + 3659.4 E-computer	0.57	0.32
	E-Stress wave	E-Static	238	E-static = 0.015 + 0.717 E-stress wave	0.76	0.58
	E-Stress wave	MOR	238	MOR = -614.1 + 2860.322 E-stress wave	0.45	0.20

Table IV. Analysis of Data for Green Tree Lumber.

Size	Abscissa	Ordinate	Number of Specimens	Regression Equation	Correlation Coefficient	Coefficient of Determination
2 x 8	E-Computer	E-Static	44	E-static = 0.036 + 0.964 E-computer	0.98	0.96
	MOR	E-Computer	24	MOR = -4,440 + 5560 E-computer	0.89	0.79
2 x 6	E-Stress wave	E-static	40	E-static = -0.105 + 1.046 E-stress wave	0.95	0.90
	E-Computer	E-Stress wave	40	E-stress wave = 0.074 + 0.969 E-computer	0.97	0.93
2 x 4	E-Computer	E-Stress wave	107	E-stress wave = 0.250 + 0.94 E-computer	0.91	0.83
	E-Computer	E-Static	107	E-static = 0.110 + 0.773 E-computer	0.79	0.62
	E-Static	MOR	107	MOR = 2416 + 2815 E-static	0.41	0.17

green wood lumber. Whereas in Figure II the regression lines for the dead wood lumber corresponds well with one another also with that for the 2x4 green wood lumber.

Several of the correlation coefficients reported in Tables II, III, and IV are lower than normally reported. This is due to the truncation of the samples of lumber reported.

CONCLUSIONS

From the data reported, it has been concluded that the nondestructive testing methods used would grade lumber that has been cut from dead lodgepole and white pine as efficiently as lumber cut from green trees.

LITERATURE CITED

1. Galligan Wm. L. 1967, R.F. Pellerin and M.T. Lentz, "Longitudinal Vibration of Logs for Prediction of Lumber Quality", A Feasibility Study conducted at Washington State University.
2. Hoyle , R.J. 1977, "Mechanical Properties of Structural Lumber-- Input Data for Reliability Analysis of the Metal Plate Truss--Phase III--Experimental," Washington State University Research Report 77/57-55.
3. Lowery, D.P. and A.L. Hearst, Jr. 1978, "Moisture Content of Lumber Produced from Dead Western White Pine and Lodgepole Pine Trees", USDA Forest Service INT-in press. Internt. For and Range Exp. Stn., Ogden, Utah.
4. Marra, G.G., R.F. Pellerin and W.L. Galligan, 1966, "Nondestructive Determination of Wood Strength and Elasticity by Vibration", HOLZ als Roh-und Werkstoff, Bd 24. S. 460-466.
5. Pellerin, R.F. and J.W. Kern, 1974, "Stress Wave Analysis of Logs", Washington State University Research Report 74/57-95.
6. Pellerin, R.F., 1965, "A Vibrational Approach to Nondestructive Testing of Structural Lumber", Forest Products Journal, Vol XV,3.

Appendix A

Data on Lumber Cut From Dead Lodgepole Pine Trees

SPEC NO	LEN (IN.)	WIDTH (IN.)	TH. (IN.)	WT. (LB)	DEN. LB/CUIN	M.C. (%)	E C	TIME M.SEC.SW	E SW	LOAD LB	MOR PSI	DEFL (IN)	MOE 10 ⁶ PSI	VISUAL GRADE
*****	***	****	***	***	*****	***	***	*****	*****	***	***	***	*****	*****
1	121.5	6.00	1.73	20.00	0.01586	7.00	1.40	569.	1.80	3500.	6491.	0.364	1.21	
2	122.9	6.00	1.73	23.50	0.01842	7.40	2.01	529.	2.41	4250.	7882.	0.215	2.04	
3	122.7	6.00	1.74	20.00	0.01561	7.40	1.18	639.	1.40	2900.	5347.	0.391	1.12	
4	123.0	5.94	1.72	21.00	0.01671	7.70	1.60	555.	1.99	3525.	6709.	0.321	1.42	
5	122.7	6.00	1.71	22.50	0.01787	7.70	1.76	551.	2.16	3875.	7270.	0.291	1.53	
6	122.7	6.00	1.71	21.30	0.01692	7.70	1.58	555.	2.02	3930.	7374.	0.264	1.69	
7	123.1	6.87	1.73	21.00	0.01435	7.50	1.21	640.	1.29	3210.	4541.	0.300	0.98	
8	122.9	6.00	1.75	21.00	0.01627	7.30	1.24	635.	1.48	1673.	3067.	0.436	0.99	
9	146.6	6.00	1.75	27.00	0.01754	8.00	1.25	770.	1.57	2275.	4171.	0.355	1.22	
10	143.8	6.00	1.72	26.50	0.01786	8.10	1.43	708.	1.89	4055.	7564.	0.282	1.57	
11	146.7	6.00	1.76	27.50	0.01775	8.20	1.77	670.	2.09	2645.	4822.	0.255	1.70	
12	147.2	6.12	1.69	24.50	0.01609	7.60	1.17	769.	1.44	1815.	3312.	0.339	1.25	
13	146.8	6.00	1.70	30.00	0.02004	8.30	1.98	648.	2.53	4320.	8153.	0.182	2.46	
14	146.7	6.13	1.71	27.00	0.01756	7.50	1.48	716.	1.81	4000.	7190.	0.230	1.81	
15	145.7	5.94	1.71	30.00	0.02027	8.30	2.04	635.	2.66	3956.	7573.	0.242	1.89	
16	147.1	6.06	1.72	24.50	0.01598	8.00	1.21	786.	1.37	2165.	3959.	0.339	1.26	
17	147.0	6.06	1.72	22.00	0.01436	7.90	0.92	840.	1.08	2630.	4809.	0.394	1.09	
18	147.1	6.06	1.71	24.50	0.01607	8.10	1.22	775.	1.42	2310.	4249.	0.348	1.24	
19	147.0	6.12	1.74	24.50	0.01565	7.90	1.00	843.	1.17	1328.	2354.	0.539	0.76	
20	146.8	5.00	1.73	21.00	0.01654	7.90	1.10	742.	1.59	2425.	6476.	0.558	1.36	
21	170.9	6.00	1.73	31.00	0.01748	7.90	1.50	822.	1.87	3030.	5619.	0.282	1.56	
22	170.7	6.18	1.73	28.00	0.01534	7.80	1.00	996.	1.12	1120.	1958.	0.479	0.84	
23	170.8	6.17	1.72	34.50	0.01903	8.20	1.72	818.	2.06	4675.	8246.	0.264	1.54	
24	170.7	6.13	1.73	30.00	0.01657	7.90	1.55	814.	1.81	2950.	5241.	0.315	1.31	
25	170.9	6.13	1.73	26.50	0.01462	7.80	0.97	950.	1.17	1030.	1830.	0.500	0.82	
26	171.0	6.06	1.74	31.00	0.01719	7.30	1.55	836.	1.78	1680.	3037.	0.327	1.29	
27	170.8	6.06	1.71	32.00	0.01808	7.50	1.09	985.	1.35	1995.	3669.	0.455	0.95	
28	170.6	6.13	1.72	28.00	0.01557	7.40	0.92	992.	1.14	2115.	3780.	0.430	0.96	
29	170.8	6.00	1.71	29.00	0.01655	7.80	1.43	822.	1.77	1620.	3039.	0.391	1.14	
30	170.8	6.13	1.74	28.00	0.01537	7.50	0.91	1066.	0.98	1712.	3024.	0.436	0.94	
31	195.1	6.06	1.70	37.50	0.01866	7.70	1.83	928.	2.05	1650.	3053.	0.255	1.70	
32	195.1	6.25	1.74	36.00	0.01697	7.80	1.35	1041.	1.48	3000.	5098.	0.318	1.21	
33	194.8	6.00	1.71	39.30	0.01966	7.50	1.41	915.	2.22	3100.	5816.	0.364	1.22	
34	194.6	6.00	1.70	33.00	0.01663	7.00	0.92	1227.	1.04	1520.	2869.	0.573	0.78	
35	195.1	6.13	1.73	32.50	0.01571	7.70	1.47	969.	1.58	4115.	7311.	0.294	1.40	
36	195.1	6.00	1.74	32.50	0.01596	7.30	1.11	1068.	1.32	1782.	3286.	0.421	1.04	
37	194.9	6.06	1.70	37.50	0.01868	7.70	1.25	1083.	1.50	1158.	2142.	0.412	1.05	
38	194.2	5.94	1.72	37.50	0.01890	7.40	1.95	921.	2.11	3725.	7089.	0.294	1.55	

***** THE FOLLOWING PRINT OUT GIVES REGRESSION LINE AND PLOTTING FOR E-STRESS WAVE(Y) VS. E-COMPUTER

REGRESSION LINE IS E-SW= -0.038+ 1.237* (E-COMPUTER)

COEFFICIENT OF DETERMINATION= 0.90

SPEC NO	LEN (IN.)	WIDTH (IN.)	TH. (IN.)	WT. (LB)	DEN. LB/CUIN	M.C. (%)	E	TIME M.SEC.SW	E	LOAD LB	MOR PSI	DEFL (IN)	MOE 10**6 PSI	VISUAL GRADE
*****	****	*****	***	***	*****	***	***	*****	*****	*****	*****	***	*****	*****
1	97.1	3.44	1.51	7.50	0.01487	6.90	1.20	490.	1.45	885.	3640.	0.645	1.07	
2	100.3	3.41	1.49	8.20	0.01609	6.60	1.62	440.	1.94	2050.	8697.	0.409	1.75	
3	98.7	3.45	1.45	8.30	0.01681	7.10	1.46	472.	1.76	1888.	8041.	0.442	1.61	
4	123.1	3.43	1.50	11.30	0.01784	6.70	1.31	655.	1.53	1390.	5789.	0.539	1.30	
5	121.4	3.42	1.49	10.10	0.01633	6.70	1.12	676.	1.31	885.	3732.	0.576	1.23	
6	121.4	3.44	1.50	9.70	0.01548	6.70	0.83	730.	1.07	580.	2402.	0.782	0.89	
7	122.4	3.48	1.47	9.40	0.01501	6.80	1.04	668.	1.23	887.	3662.	0.621	1.10	
8	122.8	3.50	1.50	9.70	0.01505	6.50	1.02	688.	1.17	965.	3860.	0.706	0.93	
9	124.4	3.44	1.49	9.50	0.01490	6.60	1.16	629.	1.38	1318.	5494.	0.627	1.11	
10	122.7	3.45	1.48	10.40	0.01660	6.80	0.95	714.	1.19	985.	4110.	0.712	0.98	
11	123.1	3.44	1.51	10.80	0.01689	6.50	1.73	553.	2.03	1265.	5203.	0.506	1.36	
12	118.9	3.44	1.50	10.40	0.01676	6.00	0.96	686.	1.31	315.	1275.	1.209	0.55	
13	123.1	3.45	1.46	10.80	0.01742	6.10	1.14	647.	1.53	1063.	4496.	0.603	1.17	
14	122.7	3.42	1.49	11.10	0.01775	6.20	1.10	713.	1.28	1000.	4217.	0.670	1.06	
15	123.1	3.44	1.48	10.50	0.01675	6.90	1.69	550.	2.03	1760.	7386.	0.455	1.54	
16	122.8	3.45	1.47	10.00	0.01606	6.30	1.12	667.	1.32	1300.	5461.	0.600	1.17	
17	123.0	3.46	1.50	9.70	0.01519	6.30	1.08	632.	1.40	695.	2845.	0.736	0.92	
18	123.1	3.42	1.47	10.00	0.01616	6.50	1.42	578.	1.77	1405.	6006.	0.527	1.36	
19	122.8	3.51	1.49	10.80	0.01526	6.60	1.28	626.	1.43	1175.	4705.	0.488	1.35	
20	123.1	3.44	1.49	10.70	0.01696	5.90	1.18	642.	1.51	1000.	4169.	0.576	1.21	
21	123.1	3.49	1.50	10.80	0.01676	6.90	1.73	567.	1.91	2350.	9454.	0.406	1.63	
22	123.1	3.41	1.48	11.00	0.01771	6.80	1.77	559.	2.08	1755.	7495.	0.379	1.90	
23	122.8	3.47	1.48	11.00	0.01744	6.60	0.90	689.	1.35	518.	2136.	1.139	0.60	
24	147.1	3.43	1.48	12.50	0.01674	6.30	1.23	755.	1.56	1160.	4897.	0.576	1.23	
25	148.6	3.46	1.49	12.20	0.01592	6.00	1.23	736.	1.56	1440.	5934.	0.509	1.35	
26	143.5	3.46	1.49	13.00	0.01757	7.10	1.72	678.	2.03	1290.	5315.	0.439	1.56	
27	148.5	3.43	1.47	12.00	0.01603	6.70	1.49	695.	1.76	1453.	6175.	0.412	1.73	
28	147.2	3.47	1.49	12.50	0.01642	7.20	1.48	688.	1.84	1924.	7882.	0.403	1.69	
29	146.6	3.49	1.44	12.60	0.01710	7.20	1.48	724.	1.73	1640.	6873.	0.433	1.59	
30	147.0	3.50	1.48	11.00	0.01445	5.90	0.94	828.	1.12	510.	2068.	0.824	0.81	
31	147.0	3.48	1.49	13.30	0.01745	7.00	1.52	751.	1.64	2230.	9083.	0.418	1.61	
32	147.0	3.44	1.50	13.00	0.01714	6.50	1.00	925.	1.06	730.	3023.	0.879	0.79	
33	147.1	3.48	1.44	12.50	0.01696	6.20	1.23	753.	1.58	592.	2495.	0.645	1.08	
34	146.9	3.47	1.47	11.60	0.01548	6.50	0.88	914.	0.98	703.	2919.	0.961	0.72	
35	147.1	3.45	1.49	12.00	0.01587	7.00	1.28	737.	1.55	1345.	5574.	0.552	1.25	
36	146.6	3.45	1.50	12.80	0.01687	6.90	1.56	707.	1.79	1160.	4775.	0.479	1.43	
37	146.5	3.40	1.49	11.00	0.01482	7.10	1.13	766.	1.34	1395.	5953.	0.621	1.39	
38	145.6	3.42	1.48	11.70	0.01588	6.90	1.46	715.	1.65	1180.	5010.	0.512	1.39	
39	146.6	3.48	1.49	12.00	0.01579	6.30	1.24	708.	1.67	940.	3829.	0.897	0.75	
40	146.1	3.45	1.50	11.20	0.01481	6.20	1.00	832.	1.13	575.	2367.	0.721	0.95	
41	146.4	3.46	1.47	13.00	0.01746	6.80	0.99	854.	1.27	1040.	4344.	0.779	0.89	
42	147.2	3.43	1.48	12.60	0.01686	6.70	1.44	738.	1.64	1798.	7590.	0.506	1.40	
43	147.2	3.47	1.45	11.70	0.01580	7.00	1.28	736.	1.54	1305.	5494.	0.479	1.46	
44	146.9	3.48	1.46	11.30	0.01514	6.20	0.93	882.	1.03	880.	3658.	0.791	0.87	
45	147.2	3.41	1.46	12.00	0.01637	6.50	1.49	685.	1.85	975.	4221.	0.521	1.40	
46	147.2	3.45	1.44	13.30	0.01819	7.00	1.54	706.	1.93	2250.	9649.	0.409	1.75	
47	146.7	3.42	1.47	13.20	0.01790	6.30	1.66	662.	2.16	2205.	0426.	0.439	1.64	
48	147.2	3.40	1.46	13.40	0.01834	7.10	1.79	667.	2.18	2195.	9559.	0.394	1.87	
49	147.2	3.41	1.48	12.10	0.01629	6.70	1.43	713.	1.70	1345.	5744.	0.545	1.32	
50	146.0	3.46	1.48	13.20	0.01766	6.50	1.20	802.	1.45	2095.	8691.	0.600	1.15	
51	146.7	3.47	1.45	11.60	0.01572	6.80	0.87	893.	1.04	811.	3414.	0.924	0.76	
52	147.2	3.50	1.49	11.60	0.01511	6.80	1.30	717.	1.56	1196.	4816.	0.509	1.30	
53	147.0	3.43	1.46	11.90	0.01617	6.60	1.08	823.	1.26	803.	3436.	0.700	1.03	
54	147.0	3.43	1.48	12.30	0.01648	6.60	0.97	863.	1.17	254.	1072.	1.448	0.49	

***** THE FOLLOWING PRINT OUT GIVES REGRESSION LINE AND PLOTTING FOR E-STRESS WAVE(Y) VS. E-COMPUTER(X)
REGRESSION LINE IS E-SW= 0.132+ 1.106* (E-COMPUTER)

Appendix B

Data on Lumber Cut From Dead White Pine Trees

SPEC NO	LEN (IN.)	WIDTH (IN.)	TH. (IN.)	WT. (LB)	DEN. LB/CUIN.	M.C. (%)	E C	TIME M.SEC.SW	E	LOAD LB	MOR PSI	DEFL (IN)	MOE 10**6 PSI	VISUAL GRADE
P 1	96.0	3.47	1.49	6.8	0.01367	6.0	1.62	414.	1.865	1920.	7866.	0.442	1.535	C
P 2	96.0	3.48	1.50	6.8	0.01355	6.0	1.53	424.	1.762	680.	2751.	0.482	1.388	C
P 3	96.0	3.47	1.50	9.0	0.01794	6.0	2.12	405.	2.557	850.	3459.	0.345	1.953	S
P 4	96.0	3.49	1.50	5.4	0.01072	6.0	1.02	465.	1.160	450.	1810.	0.755	0.879	
P 5	120.0	3.46	1.48	10.0	0.01627	6.0	1.96	503.	2.360	1720.	7135.	0.342	2.014	C
P 6	120.0	3.47	1.50	8.7	0.01393	6.0	1.13	606.	1.391	850.	3459.	0.521	1.295	F
P 7	120.0	3.48	1.49	9.6	0.01543	6.0	1.21	612.	1.511	430.	1752.	0.533	1.263	F
P 8	120.0	3.47	1.50	9.9	0.01585	6.0	1.48	570.	1.789	730.	2971.	0.455	1.484	T
P 9	120.0	3.49	1.50	9.4	0.01496	6.0	1.18	554.	1.789	165.	664.	0.000	0.000	
P 10	120.0	3.48	1.50	9.1	0.01453	6.0	1.70	522.	1.956	1495.	6049.	0.415	1.611	S
P 11	120.0	3.48	1.49	9.0	0.01446	6.0	1.04	562.	1.680	580.	2362.	0.548	1.228	
P 12	120.0	3.48	1.51	9.0	0.01427	6.0	1.72	516.	1.966	980.	3939.	0.464	1.433	FCT
P 13	120.0	3.49	1.51	8.5	0.01344	6.0	1.59	520.	1.824	1280.	5115.	0.424	1.553	T
P 14	120.0	3.49	1.51	8.5	0.01344	6.0	1.05	636.	1.219	715.	2857.	0.627	1.050	T
P 15	120.0	3.47	1.51	10.1	0.01606	6.0	0.56	583.	1.734	480.	1940.	0.618	1.084	F
P 17	120.0	3.49	1.50	9.1	0.01448	6.0	1.70	510.	2.040	750.	3017.	0.418	1.586	F
P 16	120.0	3.53	1.50	9.4	0.01476	6.0	1.91	796.	2.206	2100.	8258.	0.364	1.762	F
P 18	120.0	3.49	1.51	7.4	0.01170	6.0	1.20	574.	1.303	640.	2558.	0.591	1.115	T
P 19	120.0	3.47	1.50	9.0	0.01440	6.0	1.45	554.	1.722	1495.	6084.	0.739	0.913	S
P 20	120.0	3.46	1.47	9.8	0.01606	6.0	1.71	506.	2.300	583.	2435.	0.512	1.356	SFS
P 21	120.0	3.46	1.49	8.1	0.01309	6.0	1.49	523.	1.756	1975.	8138.	0.421	1.627	SFS
P 22	120.0	3.49	1.50	8.7	0.01385	6.0	1.40	543.	1.723	940.	3782.	0.503	1.318	
P 23	144.0	3.44	1.48	10.5	0.01432	6.0	1.44	638.	1.864	790.	3315.	0.479	1.466	S
P 24	144.0	3.45	1.48	11.3	0.01537	6.0	1.17	614.	2.159	730.	3046.	0.391	1.780	S
P 25	144.0	3.48	1.49	10.8	0.01450	6.0	1.59	631.	1.924	435.	1772.	0.524	1.285	S
P 26	144.0	3.49	1.51	10.7	0.01410	6.0	1.80	620.	1.943	770.	3077.	0.406	1.622	C
P 27	144.0	3.49	1.51	10.4	0.01370	6.0	0.97	729.	1.366	400.	1599.	0.885	0.745	F
P 28	144.0	3.48	1.49	10.8	0.01446	6.0	1.55	645.	1.842	810.	3299.	0.570	1.182	F
P 29	144.0	3.49	1.50	9.6	0.01273	6.0	1.34	646.	1.616	695.	2796.	0.533	1.243	FC
P 30	144.0	3.41	1.48	12.8	0.01761	6.0	1.42	696.	1.926	1185.	5061.	0.461	1.564	S
P 31	144.0	3.49	1.50	10.2	0.01353	6.0	1.23	685.	1.527	980.	3942.	0.564	1.177	
P 32	144.0	3.48	1.50	11.0	0.01463	6.0	1.34	672.	1.717	1110.	4491.	0.497	1.346	T
P 33	144.0	3.47	1.50	10.1	0.01347	6.0	1.25	659.	1.643	730.	2971.	0.561	1.204	T
P 34	144.0	3.48	1.50	13.1	0.01344	6.0	1.86	666.	1.605	845.	3419.	0.403	1.660	S
P 35	144.0	3.46	1.48	11.0	0.01491	6.0	1.63	626.	2.017	1690.	7011.	0.415	1.661	S
P 36	144.0	3.45	1.46	9.4	0.01296	6.0	1.05	711.	1.358	260.	1100.	1.000	0.705	
P 37	144.0	3.48	1.50	13.0	0.01729	6.0	2.12	620.	2.383	2600.	10520.	0.370	1.809	F
P 38	144.0	3.48	1.49	10.1	0.01350	6.0	1.59	605.	1.958	940.	3829.	0.461	1.462	S
P 39	144.0	3.48	1.50	11.7	0.01556	6.0	1.86	624.	2.117	2000.	8092.	0.352	1.903	
P 40	144.0	3.48	1.50	9.8	0.01303	6.0	1.32	636.	1.707	555.	2246.	0.412	1.623	S
P 41	144.0	3.48	1.50	10.8	0.01437	6.0	1.76	612.	2.032	2000.	8092.	0.433	1.544	S
P 42	144.0	3.49	1.50	10.0	0.01327	6.0	1.62	619.	1.834	1180.	4747.	0.336	1.972	S
P 43	144.0	3.44	1.47	11.8	0.01620	6.0	1.32	695.	1.777	1819.	7686.	0.415	1.702	S
P 44	144.0	3.48	1.49	11.4	0.01527	6.0	1.65	640.	1.975	1410.	5743.	0.455	1.481	S
P 45	144.0	3.48	1.50	10.1	0.01344	6.0	1.38	670.	1.585	1120.	4532.	0.506	1.322	S
P 46	144.0	3.48	1.50	11.7	0.01556	6.0	2.06	594.	2.329	523.	2116.	0.433	1.544	S
P 47	144.0	3.47	1.50	10.0	0.01334	6.0	1.14	712.	1.394	1240.	5046.	0.561	1.204	T
P 48	144.0	3.47	1.50	11.5	0.01534	6.0	1.75	639.	1.990	1415.	5758.	0.433	1.557	T
P 49	144.0	3.47	1.50	11.6	0.01547	6.0	2.01	688.	1.732	1260.	5128.	0.348	1.936	S
P 50	144.0	3.48	1.51	11.4	0.01506	6.0	1.72	624.	2.049	645.	2592.	0.521	1.275	S
P 51	144.0	3.45	1.48	11.6	0.01577	6.0	1.55	651.	1.972	680.	2837.	0.427	1.628	
P 52	144.0	3.49	1.50	11.2	0.01486	6.0	1.99	589.	2.268	1305.	5250.	0.364	1.824	F
P 53	144.0	3.49	1.51	11.2	0.01476	6.0	1.66	656.	1.816	1160.	4636.	0.458	1.440	S
P 54	144.0	3.43	1.49	11.2	0.01522	6.0	1.41	690.	1.693	930.	3899.	0.561	1.254	S

P	55	144.0	3.49	1.50	9.0	0.01194	6.0	1.19	671.	1.405	400.	1609.	0.773	0.858	F
P	56	144.0	3.48	1.50	10.5	0.01347	6.0	1.50	663.	1.683	1305.	5280.	0.515	1.298	F
P	57	144.0	3.47	1.49	11.0	0.01477	6.0	1.11	674.	1.723	375.	1536.	0.861	0.789	F
P	58	144.0	3.49	1.51	11.5	0.01265	6.0	1.07	723.	1.282	705.	2817.	0.603	1.092	C
P	59	144.0	3.49	1.50	12.7	0.01685	6.0	2.08	618.	2.337	1410.	5672.	0.324	2.045	S
P	60	144.0	3.50	1.50	11.6	0.01428	6.0	1.66	611.	2.207	165.	660.	0.000	0.000	T
P	61	144.0	3.48	1.50	12.1	0.01609	6.0	1.91	618.	2.233	1130.	4572.	0.445	1.502	C
P	62	144.0	3.47	1.49	11.2	0.01504	6.0	1.64	627.	2.027	465.	1905.	0.670	1.014	C
P	63	144.0	3.49	1.51	11.3	0.01489	6.0	1.76	619.	2.059	860.	3437.	0.467	1.412	S
P	64	144.0	3.47	1.50	9.9	0.01321	6.0	1.50	642.	1.697	330.	1343.	0.776	0.870	F
P	65	144.0	3.48	1.51	11.5	0.01520	6.0	1.57	658.	1.860	915.	3678.	0.521	1.275	T
P	66	144.0	3.42	1.47	11.4	0.01575	6.0	1.73	624.	2.142	620.	2650.	0.736	0.977	S
P	67	144.0	3.46	1.50	10.2	0.01365	6.0	1.41	648.	1.721	1350.	5526.	0.461	1.478	T
P	68	144.0	3.47	1.50	11.6	0.01547	6.0	1.53	649.	1.946	938.	3817.	0.509	1.325	F
P	69	120.0	3.47	1.50	8.9	0.01425	6.0	0.94	653.	1.226	1000.	4069.	0.606	1.113	F
P	70	168.0	3.44	1.48	12.8	0.01497	6.0	0.67	1067.	0.950	860.	3609.	1.076	0.652	T
P	71	168.0	3.49	1.50	13.6	0.01547	6.0	1.53	792.	1.781	1110.	4465.	0.627	1.057	T
P	72	168.0	3.47	1.50	13.3	0.01524	6.0	1.90	713.	2.161	1490.	6064.	0.455	1.484	T
P	73	168.0	3.45	1.50	14.5	0.01667	6.0	1.76	768.	2.043	1110.	4570.	0.455	1.510	T
P	74	168.0	3.47	1.49	11.2	0.01289	6.0	1.19	811.	1.416	742.	3040.	0.715	0.950	S
P	75	168.0	3.48	1.50	13.2	0.01505	6.0	1.53	784.	1.769	1170.	4734.	0.518	1.291	T
P	76	168.0	3.49	1.50	11.8	0.01342	6.0	1.62	703.	1.961	560.	2253.	0.530	1.251	T
P	77	168.0	3.44	1.49	11.2	0.01301	6.0	0.81	885.	1.200	628.	2618.	1.109	0.629	T
P	78	168.0	3.48	1.50	11.9	0.01370	6.0	1.51	724.	1.870	820.	3318.	0.506	1.322	T
P	79	168.0	3.46	1.50	12.9	0.01480	6.0	1.21	802.	1.662	620.	2538.	0.718	0.948	T
P	80	168.0	3.47	1.50	14.5	0.01658	6.0	1.61	788.	1.929	1430.	5819.	0.497	1.358	S
P	81	168.0	3.46	1.49	13.0	0.01501	6.0	1.82	723.	2.074	920.	3791.	0.421	1.627	S
P	82	168.0	3.48	1.50	12.8	0.01495	6.0	1.64	738.	1.936	825.	3338.	0.570	1.174	T
P	83	168.0	3.49	1.50	13.0	0.01478	6.0	1.76	733.	1.988	1846.	7426.	0.445	1.489	S
P	84	168.0	3.47	1.51	12.0	0.01363	6.0	1.13	801.	1.535	390.	1577.	0.876	0.765	S
P	85	168.0	3.49	1.50	11.6	0.01319	6.0	1.58	702.	1.934	1030.	4144.	0.476	1.394	F
P	86	168.0	3.47	1.50	12.0	0.01372	6.0	1.38	785.	1.609	845.	3439.	0.633	1.065	T
P	87	168.0	3.48	1.51	13.9	0.01574	6.0	1.60	766.	1.939	1190.	4783.	0.464	1.433	T
P	88	168.0	3.48	1.50	11.6	0.01323	6.0	1.33	766.	1.629	1550.	6271.	0.591	1.132	S
P	89	168.0	3.47	1.50	15.3	0.01750	6.0	1.75	777.	2.093	2000.	8139.	0.473	1.427	S
P	90	168.0	3.48	1.50	12.3	0.01403	6.0	1.12	863.	1.360	1500.	6069.	0.648	1.031	F
P	91	168.0	3.49	1.50	12.6	0.01436	6.0	1.14	853.	1.422	1205.	4848.	0.573	1.158	F
P	92	268.0	3.46	1.50	16.8	0.01927	6.0	1.95	784.	2.265	2350.	9619.	0.382	1.782	S
P	93	168.0	3.47	1.50	13.4	0.01532	6.0	1.38	860.	1.497	1560.	6348.	0.585	1.154	S
P	94	168.0	3.48	1.49	13.0	0.01492	6.0	1.93	692.	2.251	1190.	4847.	0.436	1.543	S
P	95	168.0	3.48	1.49	12.0	0.01377	6.0	1.13	887.	1.265	580.	2362.	0.691	0.975	F
P	96	168.0	3.48	1.50	11.7	0.01334	6.0	1.56	740.	1.760	994.	4022.	0.515	1.298	F
P	97	168.0	3.47	1.50	11.8	0.01349	6.0	1.40	756.	1.706	900.	3663.	0.542	1.244	F
P	98	168.0	3.46	1.48	10.3	0.01197	6.0	1.28	758.	1.505	1165.	4833.	0.576	1.198	F
P	99	168.0	3.46	1.48	11.5	0.01337	6.0	1.30	810.	1.472	1055.	4376.	0.576	1.198	F
P	100	168.0	3.46	1.50	12.8	0.01468	6.0	1.73	723.	2.029	1415.	5792.	0.442	1.538	S
P	101	168.0	3.47	1.50	15.4	0.01761	6.0	1.83	770.	2.146	1120.	4558.	0.427	1.579	C
P	102	168.0	3.48	1.45	15.0	0.01769	6.0	2.09	711.	2.529	2200.	9208.	0.348	1.986	C
P	103	168.0	3.54	1.49	12.4	0.01399	6.0	1.59	732.	1.886	490.	1929.	0.503	1.272	S
P	104	168.0	3.47	1.50	15.0	0.01715	6.0	1.22	873.	1.626	597.	2429.	0.621	1.086	S
P	105	168.0	3.46	1.50	12.9	0.01479	6.0	1.56	758.	1.860	1755.	7183.	0.506	1.345	C
P	106	168.0	3.47	1.49	15.8	0.01819	6.0	2.49	686.	2.793	2210.	9054.	0.318	2.135	S
P	107	168.0	3.46	1.49	13.0	0.01501	6.0	1.62	735.	2.000	1265.	5212.	0.436	1.570	S
P	108	168.0	3.49	1.50	12.5	0.01421	6.0	1.56	747.	1.840	1390.	5592.	0.461	1.440	C
P	109	168.0	3.46	1.49	13.2	0.01524	6.0	1.44	805.	1.700	1518.	6255.	0.500	1.370	S
P	110	168.0	3.47	1.49	12.7	0.01462	6.0	1.70	723.	2.021	1060.	4343.	0.485	1.401	C
P	111	168.0	3.46	1.48	12.0	0.01395	6.0	1.56	728.	1.901	1465.	6077.	0.515	1.339	S
P	112	168.0	3.45	1.49	11.4	0.01320	6.0	1.30	790.	1.528	693.	2872.	0.567	1.220	F
P	113	168.0	3.48	1.49	13.3	0.01527	6.0	1.57	745.	1.987	750.	3055.	0.579	1.163	S
P	114	168.0	3.46	1.49	12.0	0.01386	6.0	1.68	710.	1.985	1640.	6758.	0.485	1.413	C
P	115	168.0	3.46	1.49	14.6	0.01685	6.0	1.45	833.	1.755	1780.	7334.	0.500	1.370	T
P	116	168.0	3.48	1.49	14.4	0.01653	6.0	1.95	734.	2.216	1580.	6436.	0.388	1.736	T
P	117	168.0	3.45	1.45	11.5	0.01368	6.0	1.18	820.	1.470	815.	3471.	0.621	1.143	S

2118	192.0	3.46	1.50	13.0	0.01491	6.0	1.84	726	2.043	1630	6672	0.455	1.477	S
2119	192.0	3.44	1.44	12.6	0.01473	6.0	1.70	749	1.897	1950	8184	0.433	1.620	S
2120	192.0	3.45	1.49	13.1	0.01517	6.0	2.02	688	2.315	1582	6556	0.406	1.702	S
2121	192.0	3.45	1.44	12.8	0.01468	6.0	1.93	698	2.206	1350	5600	0.424	1.626	S
2122	192.0	3.46	1.48	13.4	0.01558	6.0	1.72	731	2.106	1795	7446	0.427	1.614	S
2123	192.0	3.46	1.44	14.4	0.01643	6.0	2.15	706	2.410	1860	7664	0.370	1.853	C
2125	192.0	3.47	1.49	13.2	0.01520	6.0	1.86	714	2.153	1485	6084	0.482	1.410	SC
2126	192.0	3.48	1.49	12.4	0.01433	6.0	1.38	776	1.719	1075	4379	0.597	1.128	SC
2127	192.0	3.47	1.49	12.5	0.01259	6.0	1.45	872	1.565	1705	6985	0.524	1.296	S
2128	192.0	3.47	1.49	14.5	0.01461	6.0	1.69	832	1.994	940	3851	0.533	1.274	T
2129	192.0	3.47	1.49	16.0	0.01612	6.0	1.46	916	1.815	926	3794	0.585	1.161	T
2130	192.0	3.45	1.49	13.0	0.01317	6.0	1.07	990	1.224	557	2308	0.812	0.851	T
2131	192.0	3.46	1.48	13.5	0.01373	6.0	2.03	864	1.738	2150	8919	0.482	1.432	T
2132	192.0	3.46	1.49	14.5	0.01465	6.0	1.59	846	1.934	870	3585	0.555	1.236	C
2133	192.0	3.47	1.49	15.0	0.01511	6.0	1.47	873	1.873	710	2909	0.621	1.093	T
2134	192.0	3.47	1.49	14.0	0.01410	6.0	1.76	809	2.036	960	3933	0.491	1.384	T
2135	192.0	3.47	1.49	16.5	0.01662	6.0	1.81	869	2.079	1675	6862	0.400	1.698	T
2136	192.0	3.47	1.49	13.0	0.01309	6.0	1.37	928	1.437	925	3790	0.542	1.252	T
2137	192.0	3.47	1.49	14.5	0.01461	6.0	1.81	813	2.087	456	1868	0.606	1.121	S
2138	192.0	3.48	1.49	15.0	0.01506	6.0	1.83	825	2.091	775	3157	0.494	1.363	S
2139	192.0	3.47	1.48	13.5	0.01369	6.0	1.47	885	1.651	952	3926	0.530	1.290	C
2140	192.0	3.46	1.50	15.5	0.01554	6.0	1.85	843	2.068	2240	9168	0.445	1.528	C
2141	192.0	3.46	1.49	14.0	0.01414	6.0	1.84	795	2.114	1820	7499	0.421	1.627	S
2142	192.0	3.45	1.48	15.0	0.01530	6.0	1.85	832	2.088	1730	7218	0.439	1.584	T
2143	192.0	3.46	1.49	14.0	0.01414	6.0	1.33	921	1.575	750	3090	0.558	1.229	T
2144	192.0	3.46	1.44	15.0	0.01515	6.0	1.69	857	1.950	943	3886	0.615	1.114	T
2145	192.0	3.47	1.49	15.5	0.01561	6.0	1.59	917	1.754	1158	4744	0.579	1.174	T
2146	192.0	3.44	1.49	13.0	0.01321	6.0	0.83	1116	1.002	365	1522	1.030	0.677	T
2147	192.0	3.45	1.49	16.5	0.01672	6.0	1.86	820	2.349	957	3966	0.573	1.207	F
2148	192.0	3.47	1.49	11.5	0.01158	6.0	1.16	925	1.280	1070	4384	0.627	1.083	F
2149	192.0	3.46	1.49	14.0	0.01414	6.0	1.42	875	1.745	500	2060	0.639	1.072	T
2150	192.0	3.47	1.48	15.5	0.01572	6.0	1.79	867	1.976	1020	4207	0.555	1.233	T
2151	192.0	3.41	1.46	14.0	0.01465	6.0	0.92	1100	1.143	280	1212	1.276	0.573	T
2152	192.0	3.48	1.50	14.5	0.01447	6.0	1.62	880	1.765	762	3083	0.606	1.104	T
2153	192.0	3.42	1.49	14.0	0.01431	6.0	1.13	950	1.498	432	1822	0.964	0.736	T
2154	192.0	3.47	1.48	12.5	0.01268	6.0	1.03	929	1.388	255	1052	1.515	0.451	T
2155	192.0	3.47	1.48	13.5	0.01369	6.0	1.55	838	1.841	712	2937	0.594	1.151	S
2156	192.0	3.40	1.46	13.5	0.01416	6.0	0.96	1045	1.225	582	2535	0.848	0.868	T
2157	192.0	3.48	1.49	15.5	0.01552	6.0	1.77	855	2.006	1095	4460	0.494	1.363	S
2158	192.0	3.45	1.48	15.5	0.01581	6.0	1.17	1061	1.326	580	2420	0.821	0.847	T
2159	192.0	3.48	1.50	13.0	0.01297	6.0	1.50	844	1.721	1330	5381	0.552	1.213	S
2160	192.0	3.46	1.48	16.5	0.01678	6.0	2.08	823	2.342	1520	6305	0.427	1.614	T
2161	192.0	3.48	1.50	15.5	0.01547	6.0	1.95	861	1.970	1250	5058	0.442	1.512	T
2162	192.0	3.43	1.57	14.0	0.01354	6.0	0.54	1412	0.642	620	2467	0.927	0.720	T
2163	192.0	3.46	1.49	13.0	0.01257	6.0	1.19	973	1.254	660	2720	0.606	1.130	T
2164	192.0	3.46	1.49	14.0	0.01414	6.0	1.75	834	1.921	1795	7396	0.500	1.370	S
2165	192.0	3.48	1.49	12.5	0.01256	6.0	1.13	953	1.306	430	1752	0.791	0.851	F
2166	192.0	3.46	1.50	16.0	0.01606	6.0	1.80	860	2.051	1565	6406	0.470	1.449	S
2167	192.0	3.45	1.49	14.5	0.01469	6.0	1.05	1037	1.291	1183	4903	0.645	1.071	F
2168	192.0	3.42	1.50	14.0	0.01480	6.0	1.92	830	2.029	905	3579	0.445	1.451	T
2169	192.0	3.47	1.49	17.0	0.01712	6.0	2.01	864	2.168	1150	4711	0.518	1.311	S
2170	192.0	3.49	1.50	12.5	0.01244	6.0	1.19	938	1.335	1175	4727	0.688	0.964	S
2171	192.0	3.49	1.50	14.5	0.01443	6.0	1.01	953	1.500	350	1408	1.145	0.579	F
2172	192.0	3.29	1.47	13.5	0.01454	6.0	1.26	880	1.774	362	1672	0.736	1.097	F
2173	192.0	3.46	1.49	15.0	0.01515	6.0	1.79	843	2.016	1650	6799	0.424	1.615	F
2174	192.0	3.34	1.50	15.0	0.01559	6.0	0.85	1189	1.043	175	769	0.000	0.000	F
2175	192.0	3.47	1.49	15.0	0.01511	6.0	1.30	937	1.626	950	3892	0.624	1.088	F
2176	192.0	3.47	1.49	13.0	0.01309	6.0	1.27	864	1.657	675	2765	0.591	1.149	F
2177	192.0	3.49	1.50	15.0	0.01493	6.0	1.37	957	1.540	744	2993	0.567	1.170	S
2178	192.0	3.49	1.50	14.0	0.01393	6.0	1.26	1046	1.203	535	2152	0.739	0.897	S
2179	192.0	3.50	1.50	13.0	0.01290	6.0	1.50	840	1.727	695	2780	0.588	1.118	F
2180	192.0	3.45	1.50	16.0	0.01610	6.0	1.58	916	1.814	1368	5632	0.579	1.186	S

P181	192.0	3.48	1.49	14.0	0.01406	6.0	1.29	838.	1.892	505.	205.	0.774	0.070
P182	192.0	3.47	1.49	14.5	0.01158	6.0	1.28	856.	1.493	1503.	6157.	0.658	1.033
P183	192.0	3.47	1.50	14.0	0.01401	6.0	1.86	812.	2.007	2080.	8464.	0.412	1.637
P184	192.0	3.48	1.49	15.0	0.01507	6.0	1.87	834.	2.046	1610.	6558.	0.400	1.683
P185	192.0	3.48	1.49	17.0	0.01708	6.0	1.48	913.	1.935	661.	2692.	0.564	1.195
P186	192.0	3.48	1.50	14.5	0.01443	6.0	1.69	857.	1.856	1410.	5705.	0.436	1.533
P187	192.0	3.49	1.49	14.5	0.01453	6.0	1.23	912.	1.650	446.	1806.	0.624	1.069
P188	192.0	3.47	1.49	15.0	0.01511	6.0	1.25	944.	1.602	918.	3761.	0.642	1.057
P189	192.0	3.48	1.50	12.0	0.01197	6.0	1.20	898.	1.603	505.	2043.	0.652	1.027
P190	192.0	3.48	1.49	14.5	0.01456	6.0	1.66	840.	1.950	1670.	6802.	0.455	1.481
P191	192.0	3.47	1.50	14.5	0.01451	6.0	1.56	889.	1.942	1120.	4558.	0.642	1.050
P192	192.0	3.47	1.48	13.0	0.01311	6.0	1.42	840.	1.755	820.	3382.	0.585	1.169
P193	192.0	3.49	1.50	12.5	0.01244	6.0	1.48	825.	1.726	1135.	4566.	0.564	1.177
P194	192.0	3.47	1.51	15.5	0.01541	6.0	1.93	831.	2.108	1730.	6994.	0.406	1.651
P195	192.0	3.48	1.50	13.0	0.01297	6.0	1.49	850.	1.696	1825.	7384.	0.497	1.346
P196	192.0	3.47	1.48	14.5	0.01470	6.0	1.65	818.	2.077	1550.	6393.	0.482	1.419
P197	192.0	3.44	1.48	14.0	0.01432	6.0	1.28	970.	1.438	1040.	4365.	0.633	1.108
P198	192.0	3.48	1.49	16.5	0.01657	6.0	2.16	810.	2.387	2475.	10081.	0.373	1.807
P199	192.0	3.46	1.49	14.0	0.01456	6.0	1.73	833.	1.926	1640.	6758.	0.476	1.440
P200	192.0	3.47	1.49	14.0	0.01456	6.0	1.63	852.	1.842	988.	4048.	0.515	1.319
P201	192.0	3.47	1.48	15.5	0.01572	6.0	1.31	966.	1.592	350.	1444.	1.100	0.622
P202	192.0	3.45	1.49	13.0	0.01317	6.0	1.14	942.	1.403	880.	3647.	0.682	1.014
P203	192.0	3.46	1.50	16.0	0.01606	6.0	1.78	851.	2.094	900.	3684.	0.464	1.468
P204	192.0	3.46	1.49	16.0	0.01616	6.0	2.08	810.	2.328	740.	3049.	0.412	1.662
P205	192.0	3.46	1.49	16.0	0.01616	6.0	2.07	814.	2.305	1400.	5769.	0.367	1.869
P206	192.0	3.47	1.49	14.0	0.01410	6.0	1.73	838.	1.897	2190.	8972.	0.455	1.494
P207	192.0	3.46	1.48	14.5	0.01475	6.0	0.98	1018.	1.344	796.	3302.	0.876	0.788
P208	192.0	3.47	1.49	15.5	0.01461	6.0	1.76	841.	1.951	1840.	7538.	0.430	1.579
P209	192.0	3.49	1.49	14.5	0.01452	6.0	1.54	902.	1.687	1135.	4597.	0.648	1.030
P210	192.0	3.47	1.49	16.0	0.01612	6.0	2.00	826.	2.231	1405.	5756.	0.394	1.724
P211	192.0	3.48	1.50	14.5	0.01447	6.0	1.75	850.	1.892	1670.	6757.	0.439	1.522
P212	192.0	3.48	1.49	13.0	0.01306	6.0	1.29	905.	1.506	750.	3055.	0.642	1.048
P213	192.0	3.46	1.49	19.5	0.01970	6.0	1.89	914.	2.228	1260.	5192.	0.445	1.538
P214	192.0	3.49	1.50	14.0	0.01393	6.0	1.52	896.	1.640	850.	3420.	0.567	1.170
P215	192.0	3.47	1.50	15.0	0.01501	6.0	2.05	810.	2.162	1520.	6186.	0.391	1.726
P216	192.0	3.45	1.49	15.5	0.01570	6.0	1.65	901.	1.828	1650.	6838.	0.482	1.434
P217	192.0	3.45	1.48	14.0	0.01428	6.0	1.31	1063.	1.194	1420.	5925.	0.491	1.417
P218	192.0	3.46	1.49	13.0	0.01313	6.0	1.43	911.	1.495	1400.	5769.	0.624	1.098
P219	192.0	3.45	1.48	13.0	0.01326	6.0	1.35	881.	1.613	605.	2524.	0.733	0.949
P220	192.0	3.47	1.48	14.5	0.01470	6.0	1.63	870.	1.836	2520.	10394.	0.452	1.515
P221	192.0	3.48	1.49	16.0	0.01607	6.0	1.98	826.	2.225	1840.	7495.	0.409	1.646
P222	192.0	3.48	1.49	13.5	0.01356	6.0	1.44	865.	1.712	947.	3857.	0.639	1.053
P223	192.0	3.50	1.50	14.5	0.01439	6.0	1.25	956.	1.487	1280.	5120.	0.533	1.233
P224	192.0	3.45	1.49	13.5	0.01368	6.0	1.21	936.	1.475	652.	2702.	0.673	1.027
P225	192.0	3.48	1.49	13.0	0.01306	6.0	1.50	837.	1.761	1863.	7588.	0.512	1.315
P226	192.0	3.48	1.49	16.0	0.01607	6.0	2.11	793.	2.415	1357.	5527.	0.433	1.554
P227	192.0	3.48	1.48	15.0	0.01517	6.0	2.03	796.	2.261	1340.	5495.	0.370	1.834
P228	192.0	3.47	1.49	13.5	0.01360	6.0	1.57	837.	1.833	538.	2204.	0.670	1.014
P229	192.0	3.46	1.49	15.0	0.01515	6.0	1.78	852.	1.972	1500.	6181.	0.479	1.431
P230	192.0	3.44	1.49	16.0	0.01626	6.0	2.01	837.	2.193	745.	3106.	0.488	1.429
P231	192.0	3.47	1.49	15.0	0.01511	6.0	1.89	842.	2.013	1925.	7886.	0.445	1.525
P232	192.0	3.45	1.49	14.0	0.01418	6.0	1.55	864.	1.796	650.	2694.	0.606	1.140
P233	192.0	3.47	1.49	13.0	0.01309	6.0	1.53	857.	1.685	1930.	7907.	0.518	1.311
P234	192.0	3.46	1.48	15.0	0.01526	6.0	1.65	886.	1.837	1230.	5102.	0.521	1.323
P235	192.0	3.46	1.48	15.5	0.01576	6.0	1.45	978.	1.558	1735.	7197.	0.548	1.258
P236	192.0	3.47	1.49	13.5	0.01360	6.0	1.17	876.	1.674	925.	3790.	0.588	1.155
P237	192.0	3.48	1.50	14.5	0.01461	6.0	1.64	895.	1.724	1890.	7647.	0.470	1.424
P238	192.0	3.47	1.50	13.5	0.01351	6.0	1.64	840.	1.809	917.	3732.	0.482	1.400

***** THE FOLLOWING PRINT OUT GIVES REGRESSION LINE AND PLOTTING FOR E-STRESS WAVE(Y) VS. E-COMPUTER(X)